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## **A SPECIAL CASE OF CALCULATION OF OPTICAL SYSTEM FOR A COLLIMATOR WITH AN ANFOCAL ACHROMATIC COLLIMATOR**

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*Abstract. In connection with the development of collimator for the needs of the defense, the research on mirror-lens objectives is being enhanced, especially objectives with an afocal achromatic compensator, located in parallel shaft of light with a reflector in the form of a flat plane.*

*Key words: mirror-lens objective, afocal achromatic compensator*

In connection with the development of collimators for the needs of the defense [1...5], the research on designing mirror-lens objectives has been broadened. On the basis of Methods for research of an optical system for Stand-collimator 9B852Y/CU-01 [6], a special case has been researched at which  $r_4 =$ . The system is transformed into mirror-lens objective with counter-reflector in the form of a flat mirror and an achromatic afocal compensator in a parallel beam of rays (fig. 1 and fig. 2).

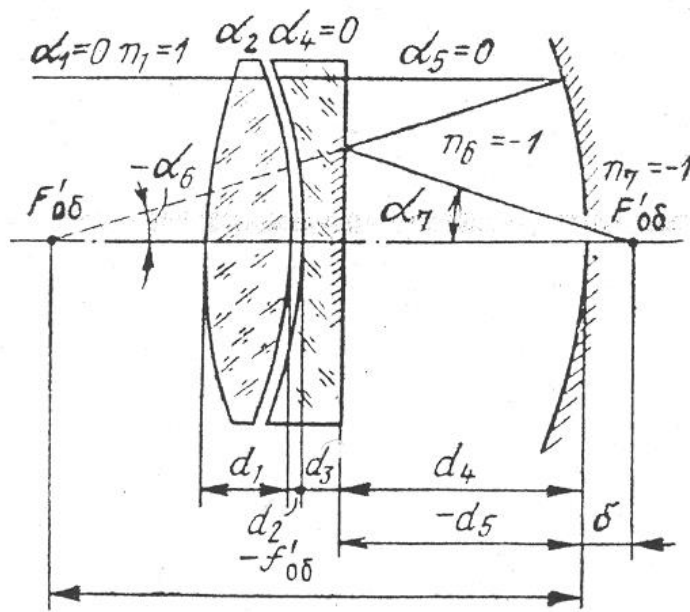


Fig. 1. Optical scheme of mirror-lens objective with an afocal achromatic compensator, located in a parallel beam of rays with counter-reflector in the form of a flat plane, put on the last plane of the compensator

Because  $r_4 = \infty$ , and the compensator is afocal, so  $\alpha_1 = \alpha_4 = \alpha_5 = 0$ . From Fig. 2 we can see that:

$$(1) \quad r_5 = 2f'_{06},$$

$$(2) \quad 2r_6 = r_4 = \infty.$$

From the similarity of the triangles  $N_5F'_{06}O_5$  и  $N_6F'_{06}P$  we can write the following:

$$(3) \quad \frac{h_5}{f'_{06}} = \frac{h_6}{f'_{06} - d_4},$$

$$(4) \quad d_4 = f'_{06} - \frac{h_6 f'_{06}}{h_5}.$$

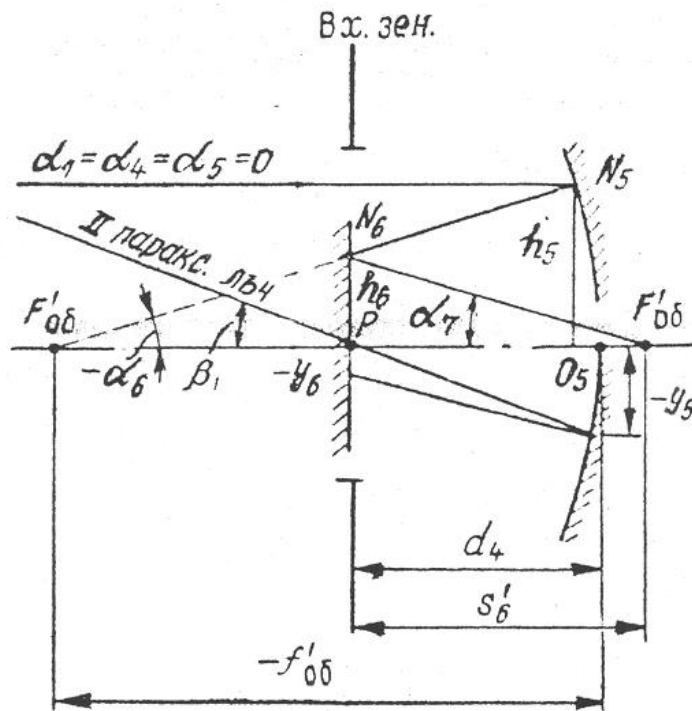


Fig. 2. Optical scheme of mirror-lens objective with an afocal achromatic compensator, located in a parallel beam of rays with counter-reflector in the form of a flat mirror

In rationing conditions  $h_5 = f'_{05} = 1$ ,  $h_6 = k$ ,  $d_4 = 1 - k$ , the values of  $S_{1огл}$  and  $S_{2огл}$  are defined [7]. Because the counter-reflector itself is a flat mirror, and  $P_6 = 0$ ,  $W_6 = 0$ , so

$$(5) \quad S_{1огл} = \sum_{v=5}^6 h_v P_v = P_5 = -\frac{\alpha_6^3}{4} = \frac{1}{4}$$

$$(6) \quad S_{2огл} = \sum_{v=5}^6 y_v P_v - I \sum_{v=5}^6 W_v = y_5 P_5 + e_5 = -d_4 \frac{1}{4} + \frac{1}{2} = \frac{k+1}{4}$$

$$(7) \quad P_{ком} = -S_{1огл} = -0,25$$

$$(8) \quad W_{ком} = -S_{2огл} = -0,25y_5 - 0,5 = 0,25d_4 - 0,5$$

Considering that  $\alpha_1 = \alpha_4 = \alpha_5 = 0$ , we get

$$(9) \quad P_{ком} = \frac{\alpha_3 \alpha_2 n}{(n-1)^2} [\alpha_2 (n+2) - \alpha_3 (2n+1)]$$

$$(10) \quad W_{KOM} = \frac{n+1}{1-n} \alpha_2 \alpha_3.$$

From (10) we define

$$(11) \quad \alpha_2 = \frac{n+1}{1-n} \frac{W_{KOM}}{\alpha_3}.$$

If we substitute the expression (11) into (10), after the transformation we get:

$$(12) \quad (1+2n)\alpha_3^2 - \left( \frac{n^2-1}{n} \right) \frac{P_{KOM}}{W_{KOM}} \alpha_3 + (n+2) \frac{n-1}{n+1} W_{KOM} = 0.$$

If we determine

$$\begin{aligned} 1+2n &= A, \\ -\frac{n^2-1}{n} \frac{P_{KOM}}{W_{KOM}} &= B, \\ (n+2) \frac{n-1}{n+1} W_{KOM} &= C, \end{aligned}$$

equation (12) can be written as this:

$$A\alpha_3^2 - B\alpha_3 + C = 0.$$

By means of solving the quadratic equation, the angle  $\alpha_3$  is defined. The order of calculation continues similarly to the Methods of calculation [6], which has been designed for Stand-collimator 9B852Y/CU-01.

In conclusion we can say that the implemented Methods for calculation of a Stand-collimator 9B852Y/CU-01 has been further developed and calculation of optical system for a collimator with afocal chromatic compensator has been ensured.

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